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Specification and Drawings, as originally filed, with Application for Patent Serial No:
2,437,047, on August 12, 2003, by KARIM S. KARIM, for "High Dynamic Range Pixel
for Digital Imaging".

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Abstract of the Disclosure

A high dynamic range pixel for digital imaging comprises a detector and a readout circuit. The detector is integrated with the readout circuit and the readout circuit has a plurality of transistors. The readout circuit is either embedded under the detector to provide a high fill factor or fabricated co-planar with the detector to reduce process complexity. A signal charge is accumulated on a pixel capacitance during an integration mode and is transferred to external electronics for data acquisition via a readout circuit during a readout mode. A pixel amplifier in the readout circuit is used to amplify low level signals while a switch is used to transfer input charge when higher level signals are detected. The pixel amplifier in the readout circuit amplifies an on-pixel sensor input signal to improve noise immunity of sensitive sensor input signals to external noise sources together with a fast pixel readout time.

HIGH DYNAMIC RANGE PIXEL FOR DIGITAL IMAGING

BACKGROUND OF THE INVENTION

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1. Field of the Invention

The present invention relates to a digital imaging system, and in particular, to a high dynamic range digital imaging pixel that can switch between large and small input signal image acquisition modes. For example, in diagnostic medical x-ray imaging applications, general digital radiography (including mammography) and low-exposure fluoroscopy, are large and small input signal modalities respectively.

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2. Description of the Prior Art

Active matrix flat-panel imagers (AMFPIS) have gained considerable significance in digital imaging, and more recently in diagnostic medical imaging applications, in view of their large area readout capability. The pixel, forming the fundamental unit of the active matrix, consists of a detector and readout circuit to efficiently transfer the collected electrons to external electronics for data acquisition. The pixel architecture most commonly used for large area X-ray imaging is the passive pixel sensor (PPS) shown in Fig. 1. Here, a detector (e.g. amorphous selenium (α -Se) based photoconductor or Cesium Iodide (CsI) phosphor coupled to an amorphous silicon (α -Si:H) p-i-n photodiode) is integrated with a readout circuit comprising an α -Si:H thin-film transistor (TFT) switch. Signal charge is accumulated on the pixel capacitance (which is either the p-i-n photodiode capacitance or an integrated storage capacitor for the α -Se photoconductor arrangement) during the integration period and is transferred to an external charge amplifier via the TFT switch during readout.

While the PPS has the advantage of being compact and thus amenable to high-resolution imaging, reading the small output signal of the PPS for low input, real-time, large area applications (e.g. fluoroscopy) requires high performance charge amplifiers. These charge amplifiers can potentially introduce noise that degrades the signal-to-noise ratio (SNR) at low signal levels thus undermining the pixel dynamic range. In particular, fluoroscopy is one of the most demanding applications for flat-panel imaging systems and relates to real-time readout. Real-time x-ray imaging or fluoroscopy is used in many medical interventional procedures where a catheter is moved through the arterial system under x-ray guidance. The technical challenge to be addressed for fluoroscopy is the need for extremely low noise, or alternatively, an increase in signal size before readout. Studies on a-Si:H PPS pixels suggest that an improvement in signal to noise ratio of an order of magnitude is desirable in order to apply these systems to more advanced imaging applications.

One approach reported to increase signal-to-noise ratio is to employ in-situ (pixel) amplification via an a-Si:H current-mediated active pixel sensor (C-APS) as depicted in Fig. 2. Here, the RESET transistor resets the pixel while the READ transistor is used to readout each pixel. The charge gain of the C-APS circuit is programmable via the transconductance of the AMP TFT, the integration time of the charge amplifier and the sensor capacitance. Gain, linearity and noise results reported show promise and indicate that the a-Si:H C-APS, coupled together with an established X-ray detection technology such as a-Se or CsI/p-i-n photodiodes, can meet the stringent requirements for digital X-ray fluoroscopy.

A primary concern with the C-APS circuit is the presence of a small-signal linearity constraint at the X-ray input. Using such a pixel amplifier for real-time fluoroscopy (where the exposure level is small) is feasible since the voltage

change at the amplifier input is also small (in mV). However, in digital chest radiography or mammography, the voltage change at the amplifier input can be much larger (in V) due to the larger X-ray exposure levels, which causes the C-APS pixel
5 output to be non-linear thus reducing the pixel dynamic range. Another consequence of a non-linear pixel transfer function is that the standard correlated double sampling mechanism cannot be implemented in hardware. Double sampling is required to correct for the effect of process non-uniformities (in the
10 form of offsets) and, in the case of a-Si:H technology, transistor stability on pixel circuit performance.

In addition, the large instability of a-Si:H transistors in the C-APS pixel at the higher supply voltages required for static radiographic applications will cause the pixel transfer
15 characteristics to shift constantly making pixel readout challenging. For supply voltages larger than 5 V, the threshold voltage of the TFTs and pixel transfer characteristics have been reported to shift significantly over time.

20 The most striking shortcoming about the C-APS pixel is that the presence of a large output current in the AMP and READ transistor branch will cause the external charge amplifier to saturate. This becomes a concern when the C-APS
25 is to be used for static radiographic applications (chest radiography, mammography) where the X-ray input and pixel output currents are both large. To implement both static and dynamic X-ray imaging, a pixel design capable of sensing a wide range of X-ray input signals is necessary.

30 SUMMARY OF THE INVENTION

Accordingly, it is an objective of the present invention to provide a high dynamic range pixel for digital imaging that is capable of amplifying sensitive sensor input signals to improve their noise immunity to external noise sources with a
35 fast pixel readout time. Concurrently, the high dynamic range

pixel is capable of reading out larger radiographic mode pixels with a fast pixel readout time.

In order to achieve the above objectives, the high dynamic range pixel in the present invention comprises a 5 detector for generating photo-carriers and discharging a certain level of induced voltage with an input signal; and a readout circuit for outputting a current or charge with respect to the induced voltage.

Preferably, the detector is either an amorphous 10 selenium(a-Se) based photoconductor or a CsI phosphor coupled to an a-Si:H p-i-n photodiode.

Further, the readout circuit has a plurality of thin-film transistors, the plurality of thin-film transistors is four 15 thin-film transistors, one of which forms part of a source follower circuit for producing an output current with respect to an input signal voltage.

The readout circuit can be embedded under the detector to provide a high fill factor or be co-planar with the detector to reduce process complexity. The readout circuit produces the 20 output current through a reset, integration and readout mode operation sequence.

BRIEF DESCRIPTION OF THE DRAWINGS

The above objective and other features of the present 25 invention will become more apparent by describing a preferred embodiment thereof with reference to the attached drawings, in which:

Fig. 1 shows a passive pixel sensor (PPS);
30 Fig. 2 shows a current mediated active pixel sensor (C-APS); and

Fig. 3 shows a high dynamic range pixel according to an implementation of the present invention.

DETAILED DESCRIPTION OF THE PREFERRED IMPLEMENTATION

The high dynamic range pixel is shown in Fig. 3. Here,
the RDC transistor is operated while the RDP is kept OFF
5 during the small, noise vulnerable, input signal acquisition
mode (i.e. fluoroscopy), and the circuit behaves as the
circuit shown in Fig 2 where there is a reset, integrate and
readout cycle. During reset, the RESET switch is turned ON to
initialize the sensor integration node (RDP and RDC are kept
OFF). During integration, photon generated charge in the
10 sensor causes a charging or discharging of the sensor node.
During integration, the RDC, RDP, and RESET switches are kept
OFF. During readout, the RDC switch is pulsed ON and a
current proportional to the induced sensor charge is output on
15 the array columns n and n-1 and the output current is
integrated by the column charge amplifiers.

For pixel operation where larger inputs can occur (i.e.
static chest radiography or mammography), the RDP pixel
transistor is operated while the RDC and RESET transistors are
20 kept OFF and the circuit operates as shown in Fig. 1 where
there is a reset, integrate and readout cycle. During
integration, photon generated charge in the sensor causes a
charging or discharging of the sensor node. During
integration, the RDC, RDP, and RESET switches are kept OFF.
25 During readout, the RDP switch is pulsed and the induced
sensor charge is transferred onto columns n-1 and n-2 and
integrated by the column charge amplifiers. The transfer of
induced charge onto the column charge amplifiers also serves
to reset the sensor integration node. If necessary, the RESET
30 switch may be used to reset the pixel after the charge is read
out.

By switching between RDC and RDP, the pixel can be used
as an amplified pixel for small, noise-vulnerable input signal
applications like X-ray fluoroscopy and as a switch based
35 pixel for higher input, imaging applications like X-ray chest
radiography or mammography. The high dynamic range pixel of

Fig. 3 is suitable for implementation in a-Si:H, poly-Si and other related technologies. The high dynamic range pixel can be interfaced to commercially available, external column charge amplifiers or be interfaced to suitable on-panel
5 fabricated column amplifiers.

Optimal layout of the additional RDP transistor and its associated bias line is needed to minimize the parasitic capacitance at the integration node so as to preserve the gain and noise performance of the amplifier circuit. The same
10 applies to the column bus capacitance that is associated with the gate and data line overlaps, since there are four transistors per pixel.

Although the preferred embodiments of the present invention have been described, it will be understood by those
15 skilled in the art that the present invention should not be limited to the described preferred embodiments, but various changes and modifications can be made within the spirit and scope of the present invention as defined by the appended claims.

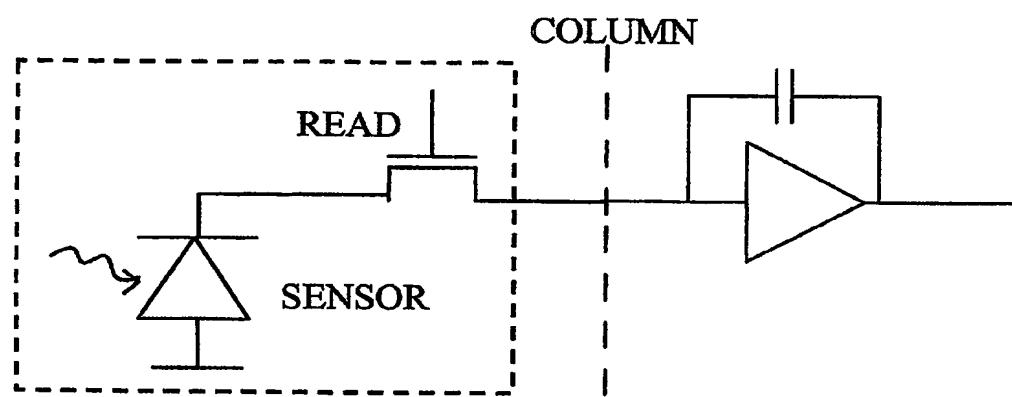


Figure 1

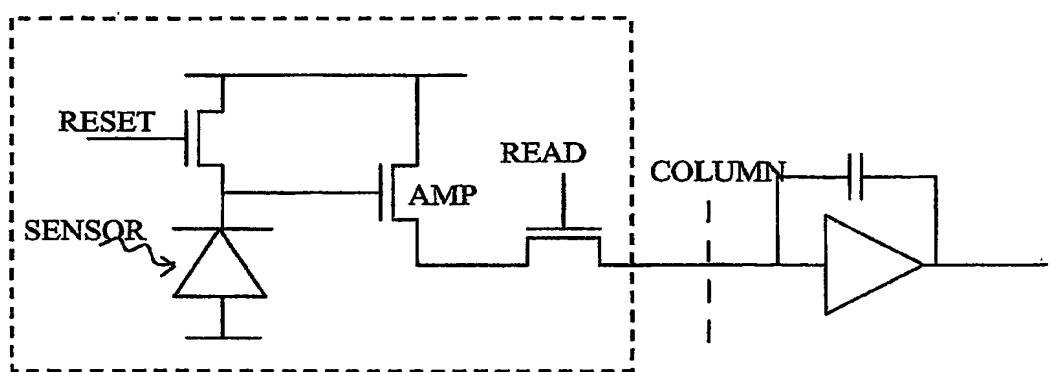


Figure 2

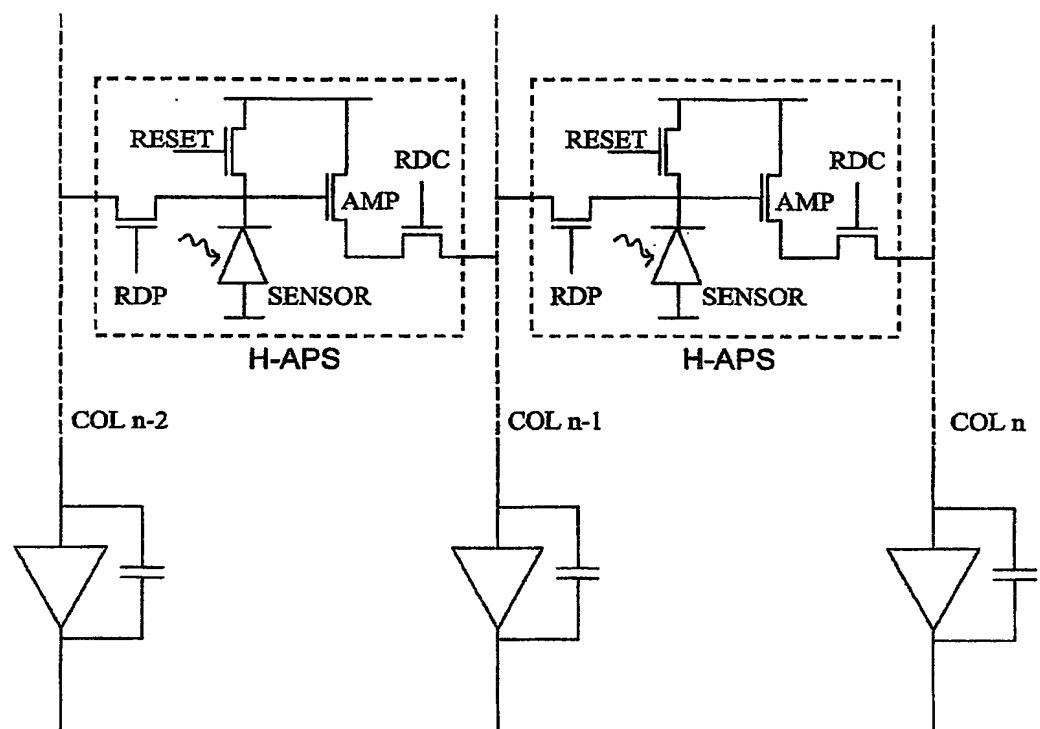


Figure 3

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